

IMPLANT INCLUDING A BODY OF NON-RESORBABLE BIOACTIVE MATERIAL

THIS INVENTION relates to an implant. It relates also to a method of making an implant.

According to a first aspect of the invention, there is provided an implant, which includes a body of non-resorbable bioactive material, with zones of resorbable bioactive material located in the body of non-resorbable material, and with the sizes of a major proportion of the zones of resorbable material being from 10 to 500 microns.

By 'size' is meant the effective cross-sectional dimension of a zone of resorbable material. When the zones are spherical, their size is thus their diameter; however, when the zones are non-circular, their size is the same as the mesh size through which such zones of resorbable material will pass.

By 'a major proportion' in respect of the zones of resorbable material that are from 10 to 500 microns, is meant at least 50% of the zones. Preferably, however, at least 80% of the zones of resorbable material are from 10 to 500 microns.

In particular, the non-resorbable bioactive material may be hydroxyapatite, while the resorbable material may be tricalcium phosphate.

The hydroxyapatite of the body is in crystalline form, and is thus substantially non-resorbable in use. The tricalcium phosphate is also in crystalline form, and may

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be in either the α or the β form, both of which are resorbable in use. However, the β or high temperature form is preferred.

5 Substantially all of the zones of tricalcium phosphate may be of the same size. The zones of the tricalcium phosphate may be randomly dispersed throughout the hydroxyapatite body. Some of the zones may thus be located at the surface of the body. The sizes of the zones may, in particular, be from 10 to 300 microns.

10 The proportion of hydroxyapatite to tricalcium phosphate in the implant may be from 4:1 to 2:3, on a mass basis, preferably about 2:1.

15 Macropores or macroporous spaces may be provided in the body. The macropores may be substantially spherical, and at least some of the macropores may be interconnected. In particular, the macropores that are interconnected may be of spherical, intercoalesced form, ie adjacent macropores may be coalesced together and thus not interconnected by elongate passageways.

20 The macropores may be from 100 to 2000 microns in size, ie may have diameters of 100 to 2000 microns, preferably 400 to 800 microns.

25 All, or at least a majority, of the macropores may be of substantially the same size. The macropores may occupy from 20% to 80% of the total volume of the body. For example, the macropores may occupy about 60% of the total volume of the body.

30 The macropores may be randomly interspersed throughout the body. Thus, the body may have a network of interconnected coalesced rounded inner macroporous spaces.

The body may also, if desired, be provided with surface concavities. The surface concavities may be rounded. The surface concavities may have diameters of from 100 to 2000 microns, preferably 200 to 400 microns, and depths of 100 to 1000 microns, preferably 200 to 500 microns, typically 200 to 400 microns.

The surface concavities may be hemispherical. The surface concavities may be interconnected with the macropores by being coalesced therewith.

If desired, micropores may also be provided in the body. While some of the micropores may also be substantially spherical, the majority of the micropores will normally be of irregular shape. The micropores may also be randomly interspersed throughout the body.

The majority of the micropores may be open micropores, ie open or connected to the surface and not necessarily connected together. The micropores may all be of substantially the same size, and may be smaller than 50 microns, ie have diameters smaller than 50 microns, preferably smaller than 10 microns.

The micropores, when present, may occupy 60% or less of the total volume of the body, excluding the volume occupied by the macropores, ie the residual volume of the body after the volume of the macropores has been excluded. Typically, the micropores may occupy about 40% of the residual body volume.

The implant is suitable for implanting into a subject. It can thus be used either as a bone implant at a site where bone growth is required, or as an implant in a site where only soft tissue is in direct contact with the implant without any bone being present in the immediate vicinity of the implant ie a soft tissue implant.

5 The hydroxyapatite and tricalcium phosphate are sintered bioactive ceramic biomaterials, and the implant has both intrinsic osteoconductivity, ie permitting bone growth into its pores or porous spaces when it is in direct contact with viable bone, and intrinsic osteoinductivity, ie permitting bone growth into its pores independently of the presence of viable bone in contact with the implant.

10 According to a second aspect of the invention , there is provided a method of making an implant, which method includes

mixing a non-resorbable bioactive material in powder form with a thermoplastic binder at elevated temperature, to produce a first powder/binder mixture;

15 comminuting the first powder/binder mixture to obtain a first granular mixture having granules or particles with sizes from 10 to 500 microns;

mixing a resorbable bioactive material in powder form with a thermoplastic binder at elevated temperature, to produce a second powder/binder mixture;

20 comminuting the second powder/binder mixture to obtain a second granular mixture having granules or particles with sizes from 10 to 500 microns;

combining the first and second granular mixtures to form a combined mixture;

25 optionally, mixing the combined mixture with fugitive phase particles which are heat decomposable, with the fugitive phase particles having sizes of 100 to 2000 microns;

30 pressing or compacting the resultant mixture into a green compact or body;

when the fugitive phase particles are present, heating the green compacts or bodies to above the decomposition temperature of the fugitive phase particles; and

35 sintering the resultant green body, to obtain an implant.

As hereinbefore described, the non-resorbable bioactive material may, in particular, be hydroxyapatite, while the resorbable material may be tricalcium phosphate.

5 Any suitable thermoplastic binder, such as a commercial polymeric binder used for extrusion or injection moulding of ceramic materials, may be used, provided it allows ambient temperature compaction of the granules to a strength adequate for further processing. The same thermoplastic binder may be used for the first and second powder/binder mixtures.

10 The temperature at which the mixing of the hydroxyapatite powder and the tricalcium phosphate powder with the thermoplastic binder to produce the first and second powder/binder mixtures takes place, depends on the thermoplastic binder used, but is typically about 120°C. The comminution of the first and second powder/binder mixtures may be effected by crushing the mixtures, and sieving them to the required granule or particle size.

15 In forming the combined mixture, the first and second mixtures are used in a desired mass ratio, depending on the desired relative portions of hydroxyapatite and tricalcium phosphate in the implant. The mixing may be effected by homogenizing the combined mixture in a ball mill without milling media, for an extended period of time, eg for a period of several hours.

20 The fugitive phase particles, when present, may be stearic acid particles, which may be substantially spherical. The stearic acid particles will be selected such that they provide macropores or macroporous spaces of a desired size in the implant. Thus, typically, stearic acid particles having a size range of 500 to 1000 microns are used.

5 The combined mixture is admixed with the fugitive phase particles in a desired mass ratio in order to provide a resultant implant having a desired macropore volume. Thus, if a desired macropore volume of approximately 60% of the total implant volume is desired, then the mass proportion of the combined mixture to fugitive phase particles will be about 1,27:1 by mass.

10 To form the green compact or body, the mixture may be pressed or compacted at a pressure of about 20MPa and machined, if necessary.

15 The temperature to which the green compacts or bodies are heated is dependent on the fugitive phase used. However, when stearic acid particles are used as the fugitive phase, the green compacts are typically heated to about 500°C, to allow melting and decomposition of the stearic acid, thereby forming in the green compacts or bodies, interconnected macropores produced by the decomposition of the stearic acid particles. The sintering is thus effected at elevated temperature, ie at a temperature above 500°C.

20 The sintering temperature and time is set or limited by the level of micropores required in the resultant implant. For example, to obtain a microporosity level or volume of 40% of the residual solid component of the implant, sintering may be effected at about 1100°C for one hour.

25 The invention will now be described in more detail, with reference to the accompanying drawing which show a cross-sectional view of an implant according to the first aspect of the invention.

30 In the drawing, reference numeral 10 generally indicates an implant according to the invention. The implant is shown as being circular in cross-section. This is for ease of illustration; in practice the implant shape and size will be dictated by its desired end use.

The implant 10 includes a body 12 of hydroxyapatite. Zones 14 of β -tricalcium phosphate are randomly dispersed throughout the body 12. The zones 14 are of approximately the same size, and have a size of about 300 microns.

- 5 The mass ratio of hydroxyapatite to β -tricalcium phosphate in the body 10 is approximately 2:1.

- 10 The body 10 also includes a plurality of randomly interspersed spherical macropores, each generally indicated by reference numeral 16. Some adjacent macropores 16 are coalesced together so that the adjacent macropores 16 are connected together by means of a connecting line 18 rather than by means of elongate tunnels or passageways. The macropores 16 are all of approximately the same size, and they have diameters in the range of 400 to 800 microns.
- 15 The macropores 16 occupy about 60% of the total volume of the body 10.

- 20 The body 10 is also provided with randomly dispersed micropores 20 having a size smaller than 10 microns. While the micropores are shown as being spherical, in practice only some of the micropores will in fact be spherical; the majority thereof will be of irregular shape as a result of incomplete sintering. The individual micropores 20 are mostly open micropores, ie open to the surface and not necessarily connected together. The micropores 20 are
- 25 dispersed throughout the body 10 as well as throughout the zones 14. The micropores 20 occupy about 40% of the residual volume of the body 12, ie the volume of the body 12 remaining after the combined volume of all the macropores 16 have been deducted from the initial volume of
- 30 the body 12.

The implant 10 is formed by compounding hydroxyapatite powder with a commercial thermoplastic polymeric binder at a temperature of about 120°C to produce a first

powder/polymer mixture. This mixture is crushed and sieved to a particle size smaller than 300 microns. In this fashion, a first granular mixture is obtained.

5 β -tricalcium phosphate powder is similarly compounded with the same thermoplastic polymeric binder at an elevated temperature of about 120°C, to produce a second powder/polymer mixture. This mixture is also crushed and sieved to a particle size smaller than 300 microns, to obtain a second granular mixture.

10 Any commercial thermoplastic polymeric binder suitable for extrusion or injection moulding of ceramic materials, may be used, provided it allows ambient temperature compaction of the granules of the mixtures to a strength adequate for further processing.

15 The first granular mixture is combined with the second granular mixture in a 2:1 ratio by mass, and homogenized by rolling thereof in a ball mill without milling media, for an extended period of several hours.

20 The resultant powder is mixed with substantially spherical particles of stearic acid which have been sieved to a size range of 500 to 1000 microns, with the mass proportion of powder to fugitive phase particles being 1,27:1. The resultant mixture is pressed or compacted at a pressure of 20MPa, and machined if necessary. In this fashion, green
25 compacts are obtained.

30 The green compacts are heated to 500°C, to allow melting and decomposition of the stearic acid particles, resulting in unsintered green compacts having interconnected coalesced macropores therein achieved by decomposition of the stearic acid particles.

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